

A DUAL ANALYSIS OF A CONTACT PROBLEM WITH FRICTION

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1 INTRODUCTION

From the variational formulation of the contact problem with friction one obtains a variational inequality of the second kind containing a non-differentiable term. One of the most used methods to remove the difficulties due to the non-differentiable term is the dualization method.

By choosing appropriate Lagrangeans one can transform the original problem of minimization, into a saddle point problem on a convex set of the form $K \times \Lambda$, where K denotes the restraints set and Λ is the Lagrange's multipliers. This new formulation enables us to use certain known algorithms in order to compute the solution and to avoid the construction of complicated convex sets and to minimize some non-differentiable functionals.

It is important to stress that the Lagrange's multipliers do have mechanical significance and may be directly approximated, in the framework of the dual problem.

The paper contains the following sections :

- existence of Lagrange's multipliers;
- existence and unicity of the saddle point of the Lagrangeans

2 VARIATIONAL INEQUALITY ARISING FROM VARIATIONAL FORM OF THE CONTACT PROBLEM

The variational form of the contact problem with friction is the following variational inequality of the second kind:

Find $u \in V$ such that

$$b(u, v - u) + j_T(v) - j_T(u) \geq L(v - u), \quad \forall v \in V \quad (1)$$

with $b(u, v) = a(u, v) + j_N(u, v)$, where:

- $V = \{v \in (H^1(\Omega))^d : v = 0 \text{ on } \Gamma_D\}$ is the functions space;
- $\Omega \subset \mathbb{R}^d$, $d = 2$ or $d = 3$ is an elastic body which occupies an open bounded Lipschitz domain, that come in contact with the rigid foundation.
- $\Gamma = \partial\Omega = \Gamma_D \cup \Gamma_N \cup \Gamma_C$ is the Lipschitz continuous boundary of the Ω ,
- $a(u, v) = \int_{\Omega} \sigma(u) \varepsilon(v) dx$ is the virtual work produced by action of the stress σ on the strain ε ;
- $j_N(u, v) = \int_{\Gamma_C} c_n (u_n - g)_+^{m_n} v_n ds$ is the virtual work produced by normal pressure on the contact boundary Γ_C ;
- $j_T(u) = \int_{\Gamma_C} c_t |j_T(u)| ds$ is the virtual work produced by tangential pressure on the contact boundary Γ_C ; with $j_T = (u_t - g)_+^{m_t}$, $g \geq 0$ is the initial gap between Γ_C and the foundation, j_T is the non-differentiable functional;
- $L(v) = \int_{\Omega} F v dx + \int_{\Gamma_D} T v ds$ is the virtual work produced by the volume force F in Ω and by the surface traction T on Γ_D ;
- c_n, c_t, m_n, m_t are material constants depending on boundary contact properties, and $(\cdot)_+ = \max(\cdot, 0)$;

We denote the multiplier space:

$$\Lambda = \left\{ \lambda \in (L^2(\Gamma_C))^{d-1} : |\lambda| \leq 1 \text{ on } \sup p p_T, \lambda = 0 \text{ on } \Gamma_C - \sup p p_T \right\} \quad (2)$$

and the restrains set:

$$K = \{v \in V : v_n \leq g\}$$

The existence of a multiplier for the problem (1) is given by

Theorem 2.1. The function $u \in V$ is the solution of the problem (1) if and only if there exists a λ , such that

$$b(u, v) + \int_{\Gamma_C} c_T p_T \lambda v_T ds = L(v), \quad \forall v \in V \quad (3)$$

$$\lambda \in \Lambda, \lambda v_T = |v_T|, \text{ on } \Gamma_C \quad (4)$$

Proof. Let $u \in V$ be the solution of the problem (1). By taking $v = 0$ and $v = 2u$ in (1), we obtain

$$b(u, v) + J_T(u) = L(u) \quad (5)$$

This, from (1) we have

$$b(u, v) + J_T(v) \geq L(v) \quad \forall v \in V$$

Hence,

$$|L(v) - b(u, v)| \leq \int_{\Gamma_C} c_T p_T |v_T| ds, \quad \forall v \in V$$

Therefore, there exists a continuous linear functional h on $H^{-1/2}(\Gamma_C)$, such that

$$\begin{aligned} L(v) - b(u, v) &= h(v_T) \\ |h(v_T)| &\leq c \|v_T\|_{H^0(\Gamma_C)} \end{aligned}$$

By Hahn-Banach Theorem, we have the existence of a $\lambda \in L^2(\Gamma_C)$ a.i.

$$\|\lambda\|_{L^2(\Gamma_C)} \leq 1$$

and

$$h(v_T) = \int_{\Gamma_C} c_T p_T \lambda v_T ds, \quad \forall v_T \in H^{1/2}(\Gamma_C)$$

i.e. we have relation (3). By taking $v=u$ in (3) we obtain

$$h(u, u) + \int_{\Gamma_C} c_T p_T \lambda u_T ds = L(u)$$

which, combining with (5), gives

$$\int_{\Gamma_C} c_T p_T (\lambda u_T - |u_T|) ds = 0.$$

It then follows that $\lambda u_T = |u_T|$ on Γ_C . Conversely, let u, λ satisfying (3), (4). In (3), we replace v by $v-u$ to obtain

$$h(u, v-u) + \int_{\Gamma_C} c_T p_T \lambda v_T ds - j_T(u) - L(v-u) = 0, \forall v \in V \quad (6)$$

Since

$$\int_{\Gamma_C} c_T p_T \lambda u_T ds \leq \int_{\Gamma_C} c_T p_T |u_T| ds$$

the relation (6) implies (1). Q.E.D.

3 VARIATIONAL INEQUALITY FORMULATION AS A SADDLE POINT PROBLEM

Following procedure from Cea and Glowinski [4], we define a Lagrangian L on $K \times \Lambda$.

Theorem 3.1 Let $u \in K, \lambda \in \Lambda$ satisfying (3) and (4). Then, (u, λ) is the unique saddle point of L on $K \times \Lambda$.

Proof. We first prove that if (u, λ) satisfy (3), (4), then (u, λ) is a saddle point of L on $K \times \Lambda$, i.e.

$$L(v, \eta) \leq L(u, \lambda) \leq L(v, \lambda), \forall v, \eta \in K \times \Lambda \quad (7)$$

The first inequality in (7) holds trivially, for

$$\int_{\Gamma_C} c_T p_T \eta v_T ds \leq \int_{\Gamma_C} c_T p_T |\eta_T| ds = \int_{\Gamma_C} c_T p_T \lambda v_T ds \quad \forall \eta \in \Lambda$$

As for the second inequality in (7), we must show that

$$\frac{1}{2}h(u, u) - L(u) + \int_{\Gamma_C} c_T p_T \lambda u_T ds < \frac{1}{2}h(v, v) - L(v) + \int_{\Gamma_C} c_T p_T \lambda v_T ds \quad \forall v \in V \quad (8)$$

Since from (3),

$$\int_{\Gamma_C} c_T p_T \lambda (v_T - u_T) ds = L(u - v) - h(u, u - v)$$

it easily seen that (8) holds.

We have proved that (u, λ) is a saddle point of L on $K \times \Lambda$. Let us now prove the uniqueness of a saddle point of L . Assume (v, λ_1) is a saddle point of L . We need to show that $v = u, \lambda_1 = \lambda$. From the first inequality in (7), we have

$$\int_{\Gamma_C} c_T p_T \eta v_T ds \leq \int_{\Gamma_C} c_T p_T \lambda v_T ds \quad \forall \eta \in \Lambda$$

In particular, taking $\eta = \lambda_1$, we obtain

$$\int_{\Gamma_C} c_T p_T (\lambda_1 - \lambda) v_T ds \leq 0 \quad (9)$$

Similarly, since (v, λ_1) is a saddle point of L , we have :

$$\int_{\Gamma_C} c_T p_T \eta v_T ds \leq \int_{\Gamma_C} c_T p_T \lambda_1 v_T ds \quad \forall \eta \in \Lambda$$

In particular, taking $\eta = \lambda$, we obtain

$$\int_{\Gamma_C} c_T p_T (\lambda - \lambda_1) v_T ds \leq 0 \quad (10)$$

Adding (9) and (10), we get

$$\int_{\Gamma_C} c_T p_T (\lambda - \lambda_1) (u_T - v_{1T}) ds \leq 0 \quad (11)$$

From the second inequality in (7), we see that

$$\theta(u, v) - L(v) + \int_{\Gamma_C} c_T p_T \lambda_1 v_T ds = 0 \quad \forall v \in K \quad (12)$$

Taking $v = v_1 - u$, we get

$$\theta(u, v_1 - u) - L(v_1 - u) + \int_{\Gamma_C} c_T p_T \lambda_1 (v_{1T} - u_T) ds = 0 \quad (13)$$

Similar, we have

$$\theta(v_1, v) - L(v) + \int_{\Gamma_C} c_T p_T \lambda_1 v_T ds = 0 \quad \forall v \in K \quad (14)$$

and

$$\theta(v_1, v_1 - u) - L(v_1 - u) + \int_{\Gamma_C} c_T p_T \lambda_1 (v_{1T} - u_T) ds = 0 \quad (15)$$

Subtracting (15) from (13), we obtain

$$\theta(v_1 - u, v_1 - u) = \int_{\Gamma_C} c_T p_T (\lambda_1 - \lambda) (u_T - v_{1T}) ds = 0$$

which by (11) is nonpositive. Hence, we must have

$$v_1 - u \quad (16)$$

Using (12), (14) and (11), we obtain

$$\int_{\Gamma_C} c_T p_T (\lambda_1 - \lambda) u_T ds = 0 \quad \forall u_T \in H^{1/2}(\Gamma_C)$$

from which, we then have

$$\lambda_1 = \lambda$$

Q.E.D.

An consequence of Theorem 2.1 and 3.1 is

Proposition 3.1. For the solution u of the problem (1), there exists a unique $\lambda \in \Lambda$, with $\lambda \nu_T = | \nu_T |$, such that

$$b(u, v) = L(v) + \int_{\Gamma_C} c_T p_T \lambda \nu_T ds \quad \forall v \in K$$

Remarks.

The relationship between the solution of problem (1), denoted by \hat{u} , on a hand, and the saddle point (u, λ) of the Lagrangean (8), by the other hand, is given by

$$\hat{u} = u \quad \text{in } \Omega, \quad \sigma_T(u) = -c_T p_T \lambda \quad \text{a.e. on } \Gamma_C \quad (17)$$

Therefore the contact problem with given friction can be approximated by solving the saddle point problem (7). This means the a minimization problem which contains a non-differentiable functional has been replaced by an other one in which the Lagrangean is regular with respect to each variable. From (17) we can deduce a very important mechanical interpretation for the Lagrange's multipliers.

One other benefit of this formulation consists in the possibility of exploiting of an Uzawa-type algorithm for the solution of the problem (7), which have to simultaneously compute the displacements as well as the contact tangential stresses.

REFERENCES

- [1] W. Han, Finite element analysis of a holonomic elastic-plastic problem, *Numer. Math.* 60, 493-508(1992)
- [2] F. Brezzi, M. Fortin, *Mixed and Hybrid Finite Element Methods*, Springer-Verlag, Berlin, 1991

[3] N.Pop, A numerical formulation for quasistatic frictional contact problem, *Proceedings 8th Int. Conf. on Difference eq. and Appl.*, Univ. of Veszprem, 1-11 aug.1995, *Gordon and Breach Publishers* (to appear)

[4] J.Cés.,R.Glowinski, Methodes numeriques pour l'écoulement laminaire d'un fluide rigide viscoplastique incompressible, *Int.J. Comput.Math.Sect. B.3*, 225-255

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